

RING FIN ROCKET CENTER OF PRESSURE, DRAG AND LIFT SLOPE  
COEFFICIENTS MEASURED USING THE AEROROCKET WIND TUNNEL

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Several ring fin rocket designs were tested in the AeroRocket wind tunnel to determine drag coefficient,  $C_d$  center of pressure location,  $X_{cp}$  and lift slope coefficient,  $C_{Na}$  verses rocket angle-of-attack. Results of these measurements are displayed in Figure-1 which provides ring fin rocket wind tunnel aerodynamic coefficients  $C_d$ ,  $X_{cp}$  and  $C_{Na}$  verses length ratio,  $L_{ring}/L_{body}$  for three cases of diameter ratio,  $D_{ring}/D_{body}$ . Curve-fit data are displayed in Figure 2, Figure-4, and Figure-5 which display  $C_d$ ,  $X_{cp}$  and  $C_{Na}$  for four ring-fin wind tunnel models. Each of the four models are 12.625 inches long and have a body tube that is 0.544 inches in diameter. The first model has a 1.594-inch diameter x 2.438-inch-long ring-fin positioned with the trailing edge of the ring-fin flush with the rear of the rocket. Similarly, model 2 was tested with its 1.594-inch diameter ring-fin, first with the ring-fin 4.875 inches long then 2.438 inches long, 1.25 inches long and finally 0.469 inches long. Model 3 was tested with its 2.219-inch diameter ring-fin, first with the ring-fin 6.688 inches long, then 3.375 inches long, 1.625 inches long and finally 0.625 inches long. Finally, model 4 was tested with its 2.594-inch diameter ring-fin, first with the ring-fin 7.875 inches long, then 4.0 inches long, 2.0 inches long and finally 0.75 inches long.

For  $C_{Na}$  measurements, each wind tunnel model with its ring-fin diameter and ring-fin length was tested at 0-degrees, 5-degrees, 10-degrees and 15-degrees angle-of-attack. Temperature and wind tunnel velocity was recorded before each measurement to determine air density and air viscosity for Reynolds number computation. Reynolds number is based on model length while the aerodynamic coefficients are referenced to the body tube cross-sectional area behind the nose cone. Center of pressure location,  $X_{cp}$  is normalized by the total body tube and nose cone length of 12.625 inches for all the wind tunnel models. The measured raw data by itself is useless unless put into a form useful for aerodynamic prediction. Therefore, all aerodynamic coefficients were curve-fit using algebraic equations as a function of ring-fin length ratio,  $L_{ring}/L_{body}$  and ring-fin diameter ratio,  $D_{ring}/D_{body}$ . Using methods of interpolation, the drag coefficient,  $C_d$ , center of pressure location,  $X_{cp}$  and lift slope coefficient,  $C_{Na}$  were curve-fit using the mathematical capability of Mathcad. There are three equations one for each aerodynamic coefficient described above, one equation for each model tested having a specific ring-fin diameter ratio,  $D_{ring}/D_{body}$ . Curve-fit equations that describe,  $C_d$ ,  $X_{cp}$  and  $C_{Na}$  are Equation-1, Equation-2, and Equation-3 respectively. In these curve-fit equations S1 and S2 were defined using AeroRocket wind tunnel measured data. Each aerodynamic coefficient is described by curve-fit equations corresponding to one of the following ring-fin diameter ratios.  $D_{ring}/D_{body} = 2.93$ ,  $D_{ring}/D_{body} = 4.08$  and  $D_{ring}/D_{body} = 4.77$ . Each aerodynamic coefficient,  $C_d$ ,  $C_N$ , and  $C_{Na}$  is a function of  $L_{ring}/L_{rocket}$  and  $D_{ring}/D_{rocket}$  derived by one of the three curve-fit equations. If the specified diameter ratios are not sufficient simply use the interpolation procedure described in Figure-7 to interpolate between diameter ratio curves. The aerodynamic coefficients are determined by interpolating between ring-fin diameter ratio curves to determine the aerodynamic coefficients. Figure-7 displays graphically how interpolation between coefficient curves is used to determine  $C_d$ ,  $X_{cp}$  and  $C_{Na}$  for new designs.

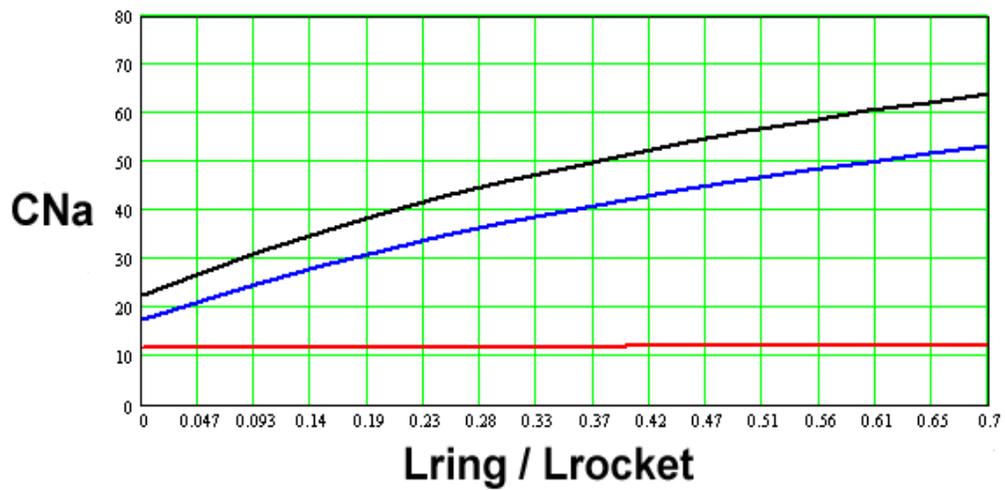
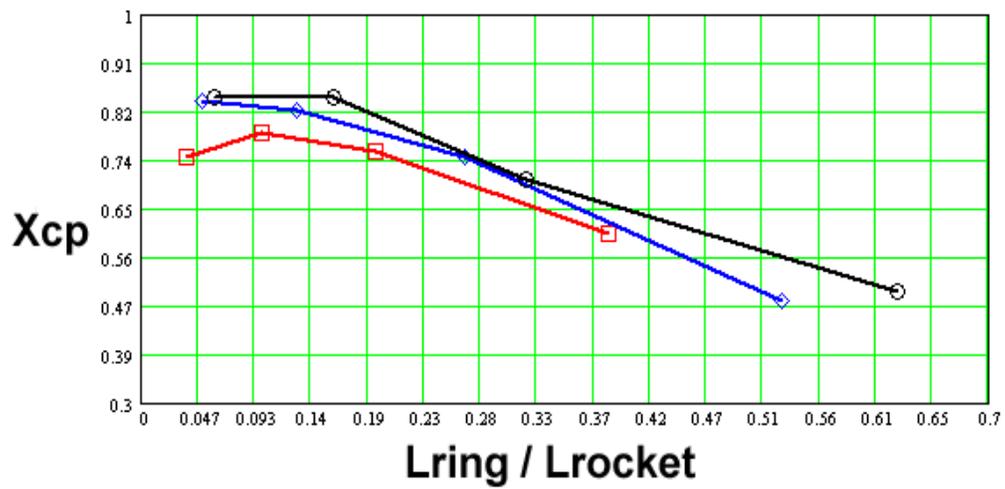
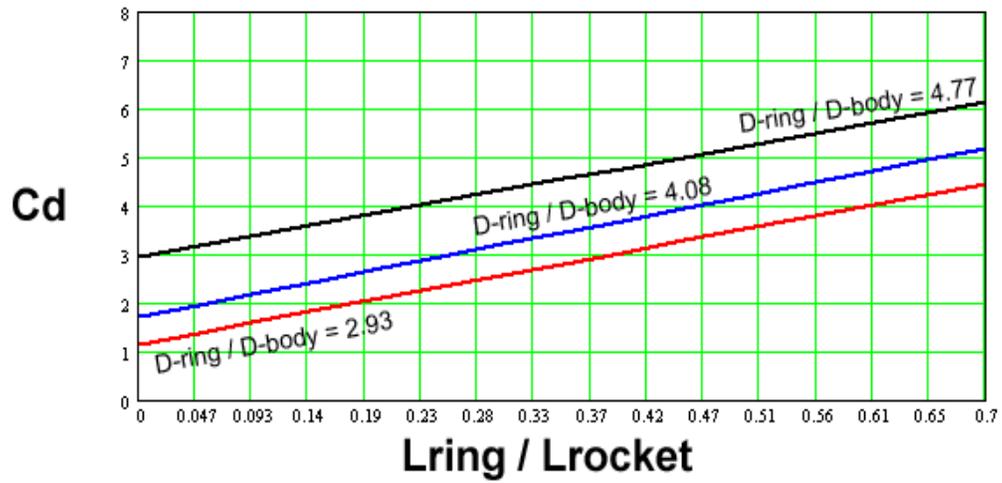


Figure-1  $C_d$ ,  $X_{cp}$  and  $C_{Na}$  curve-fit results from wind tunnel tests

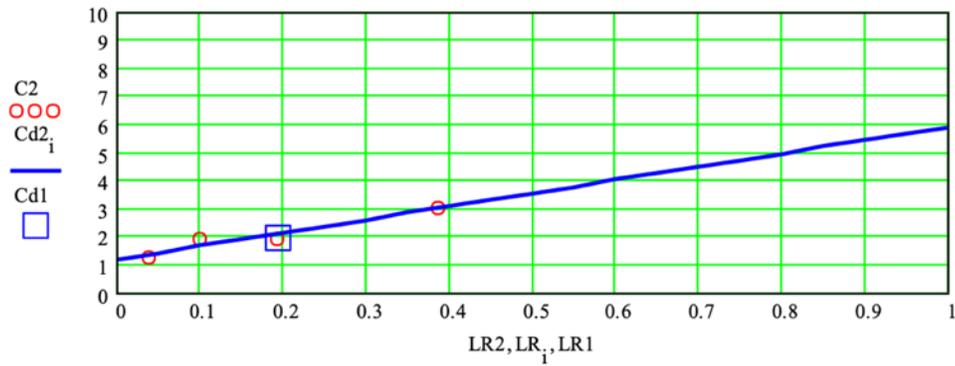
## RING FIN DRAG COEFFICIENT, Cd

Cd vs. Lring / Lrocket. Ring-Fin Cd (**0.0-degree** AOA w/o body)

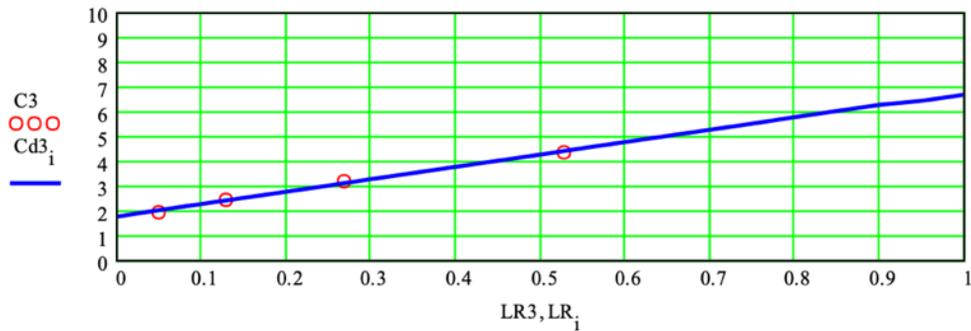
Dring / Dbody	<b>2.93</b>	<b>4.08</b>	<b>4.77</b>
<b>S1</b>	4.717786	4.954520	4.586682
<b>S2</b>	1.146967	1.709692	2.933179

$$C_d = S_1 \frac{L_{ring}}{L_{body}} + S_2 \quad (1)$$

D-ring/D-body = 2.93



D-ring/D-body = 4.08



D-ring/D-body = 4.77

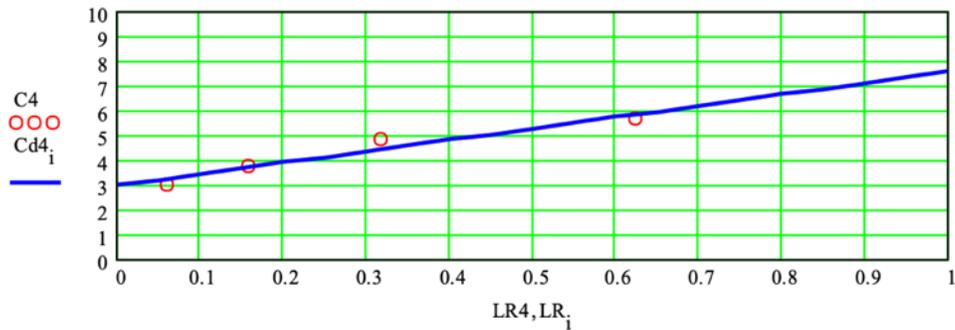


Figure-2, Rocket Cd vs Lring / Lrocket at 0-degree AOA for data and curve-fit

## CENTER OF PRESSURE LOCATION, $X_{cp}$

Center of pressure location measurements are performed using a special  $X_{cp}$ -Caliper that secures the model in the wind tunnel test section using two opposing low friction points. Figure-3a illustrates a ring-fin model rocket being tested in the AeroRocket wind tunnel for measuring center of pressure location. The ring-fin model in this configuration is stable because the support point is ahead of the actual center of pressure. The actual center of pressure location,  $X_{cp}$  is determined by moving the sting support location rearward until the model becomes unstable and "noses over" to one side or the other when the wind tunnel is operating. Figure-3b further illustrates how the ring-fin rocket model is secured in place during center of pressure location testing. Please notice the pitot tube used to measure the difference between static pressure and dynamic pressure for determining flow velocity in the wind tunnel. An analog velocity meter is used to convert the resulting pressure differential to test section flow velocity measured as 3,500 in feet per minute.

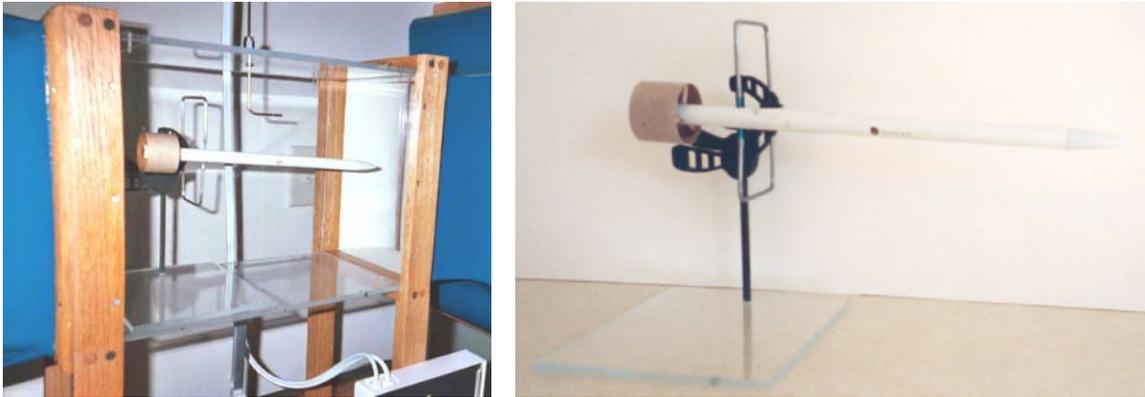


Figure-3a, Figure-3b,  $X_{cp}$  caliper uses two opposing low friction points to determine center of pressure

### MATHCAD CURVE-FIT ANALYSIS COEFFICIENTS

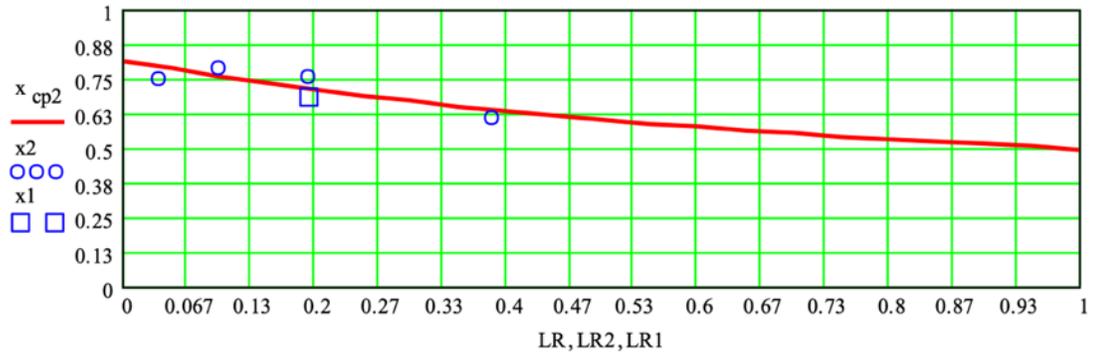
$D_{ring}/D_{rocket}$	<b>2.93</b>	<b>4.08</b>	<b>4.77</b>
$D_i/D_o$	0.34	0.25	0.21
<b>S1</b>	0.639859	1.219973	1.137153
<b>S2</b>	0.172234	-0.276811	-0.178476

Ring Fin S1 and S2 coefficients for various  $D_{ring}/D_{rocket}$

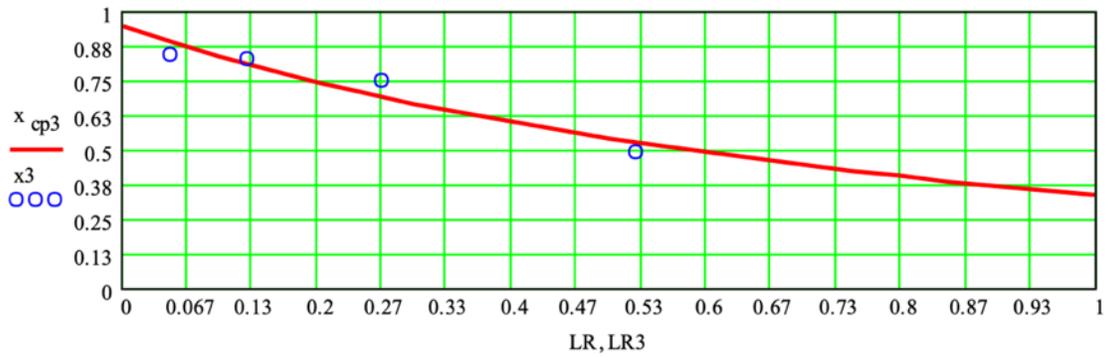
### CENTER OF PRESSURE ESTIMATION EQUATION

$$\frac{X_{cp}}{L_{rocket}} = S_1 \frac{L_{rocket}}{L_{ring} + L_{rocket}} + S_2 \quad (2)$$

D-ring/D-body = 2.93



D-ring/D-body = 4.08



D-ring/D-body = 4.77

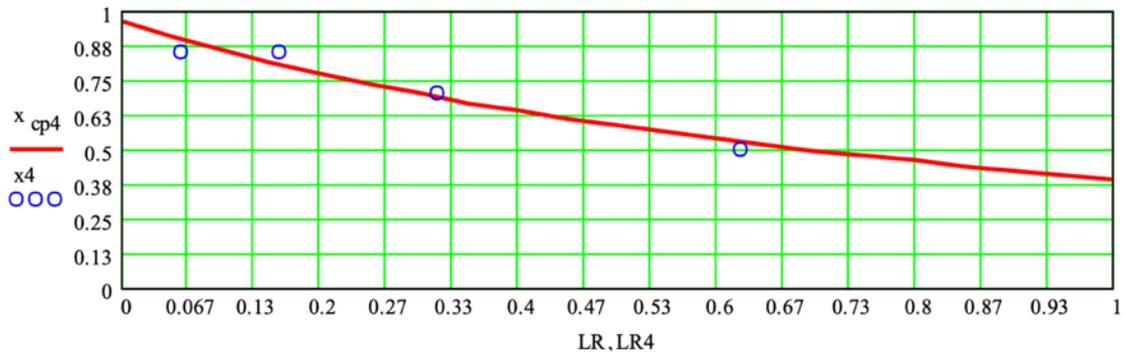


Figure-4, Rocket Xcp vs Lring / Lrocket for data and curve-fit

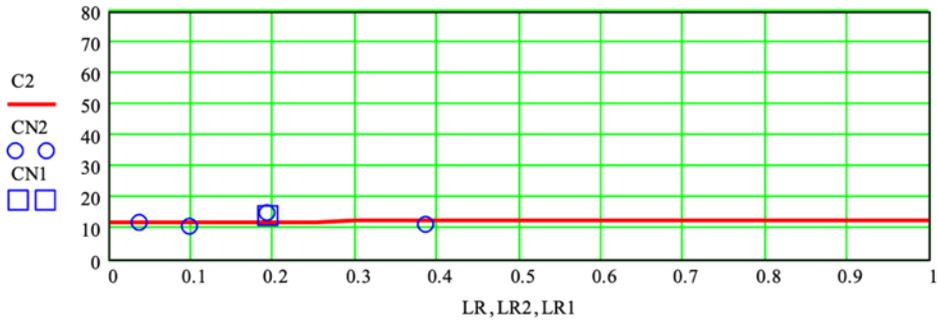
## RING FIN LIFT SLOPE COEFFICIENT, $C_{Na}$

Ring Fin  $C_{Na}$  (w/o nose).  $C_{Na}$  vs.  $L_{ring} / L_{rocket}$

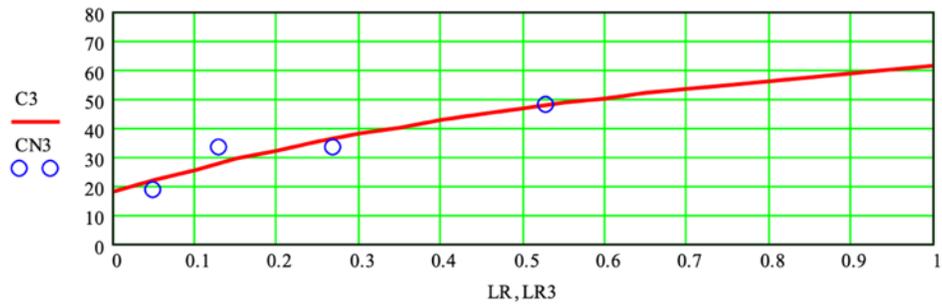
<b><math>D_{ring} / D_{body}</math></b>	<b>2.93</b>	<b>4.08</b>	<b>4.77</b>
<b>S1</b>	-1.021229	-86.783769	-101.05531
<b>S2</b>	12.671390	104.146040	123.546993

$$C_{Na} = S_1 \frac{L_{body}}{L_{ring} + L_{body}} + S_2 \quad (3)$$

D-ring/D-body = 2.93



D-ring/D-body = 4.08



D-ring/D-body = 4.77

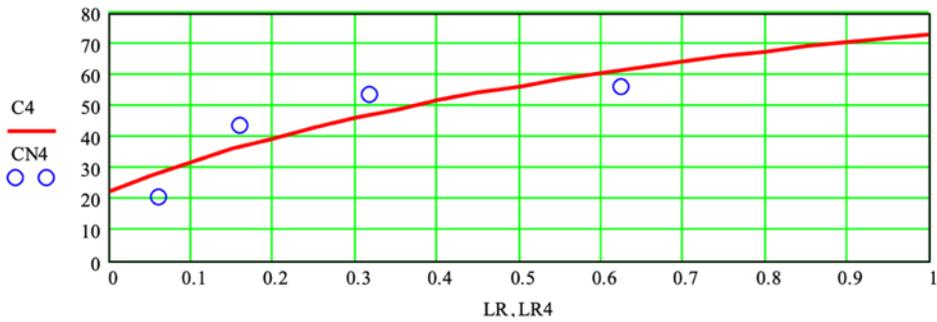


Figure-5, Ring Fin  $C_{Na}$  (w/o nose) vs.  $L_{ring} / L_{rocket}$  for data and curve-fit

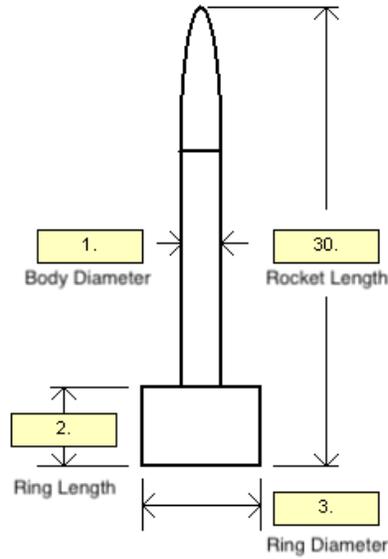


Figure-6, Ring fin geometry

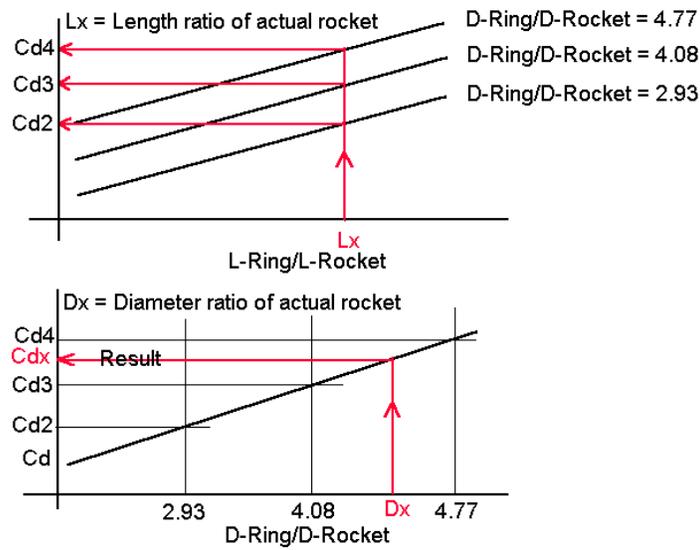


Figure-7, Ring Fin Interpolation methodology

### Classical Barrowman Ring Fin $X_{cp}$ Analysis

$$C_{N_{a \text{ nose}}} = 2.0 \quad (4)$$

$$X_{cp \text{ nose}} = 0.667 L_{\text{nose}} \quad (5)$$

$$X_{cp \text{ fin}} = \frac{1}{4} c, \text{ Location of ring fin aerodynamic center} \quad (6)$$

$$X_{cp} = \frac{C_{N_{a \text{ nose}}} X_{cp \text{ nose}} + C_{N_{a \text{ fin}}} X_{cp \text{ fin}}}{C_{N_{a \text{ nose}}} + C_{N_{a \text{ fin}}}} \quad (7)$$

$$C_{d \text{ nose-body}} = 0.305, \text{ measured rocket drag without ring fin} \quad (8)$$

## REFERENCES

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- <sup>3</sup>Frank M. White, Fluid Mechanics, (McGraw-Hill, New York, 2010)
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- <sup>7</sup>John D. Anderson, Fundamentals of Aerodynamics (McGraw-Hill, New York, 1979)